Sub-Category 2Mainly cumulative landscape values such as woods, groups,
avenues, lines.Sub-Category 3Mainly cultural values such as conservation, commemorative or
historical links.

Table 1 – Tree Data Table

No.	Species	Age	Con	Ht	CH	Ν	E	S	W	Stm	Dia	RPA	Structural Condition	PMR	Yrs	Cat
TGA	Tree Group A Himalayan Birch <i>(Betula utilis)</i>	S	G/F	4.50-5.00	1.80	0.50	0.50	0.50	0.50	1	0.60	0.76	A Group of 9, recently planted Himalayan Birch. Tree is located within circa 1 m wide roadside landscape reserve. Majority of trees appear to be in good overall condition however small stature would allow for ready replacement with new stock.		L	C2
TGB	Tree Group B Hornbeam (Carpinus betulus)	S	G/F	4.00	1.75	0.35	0.35	0.35	0.35	1	70	0.84	A group of 9 young Hornbeam's recently planted in conjunction with existing site context. Trees appear to be maintaining good general vigour and vitality however, small stature would allow for ready replacement.		L	C2
TGC	Tree Group C Oak (Quercus robur)	S	G/F	5.00	1.75	1.25	1.25	1.25	1.25	1	153	1.83	A group of 3 trees planted in conjunction with existing landscape. All trees remain vigorous however westernmost tree has suffered basal damage and is conflicting with the existing pavement. Small stature would allow for ready replacement.		L	C2
TGD	Tree Group D Horse Chestnut (Aesculus hippocastanum)	S	F	4.50	2.00	1.50	1.50	1.50	1.50	1	153	1.83	3 young and vigorous but small stature trees. Western and northern-most trees have suffered substantial basal damage. Small stature allows for ready replacement.		L	C2

No.	Species	Age	Con	Ht	СН	N	E	S	W	Stm	Dia	RPA	Structural Condition	PMR	Yrs	Cat
TGE	Tree Group E Lime <i>(Tilia europea)</i>	S	G/F	5.00	2.00	2.25	2.25	2.25	2.25	1	172	2.06	Young and vigorous, comprising typical element of existing landscape. Small stature allows for ready replacement.	r	L	C2
TGF	Tree Group F Hornbeam <i>(Carpinus betulus)</i>	S	G/F	3.50-500	3.00	1.00	1.00	1.00	1.00	1	127	1.53	An element of formal planting where trees arise from within hedging or shrub planting. Whilst there is significant variation in tree size and potentially tree vigour, a clear majority of trees appear to be in good general condition. Notwithstanding the above, small stature would allow for ready replacement.		L	C2
TGG	Tree Group G Beech Hedge (Fagus sylvatica)	S	G/F	2.00	0.00	N/A	N/A	N/A	N/A	1	95	1.15	Four sections of Beech hedging planted in conjunction with raised planters. Trees have been formally proved to create prismatic effect. Small stature would allow for replacement.	,	L	C2
TGH	Tree Group H Hornbeam <i>(Carpinus betulus)</i>	S	F	3.50-500	3.00	1.00	1.00	1.00	1.00	1	127	1.53	Young trees planted within contex of raised planters. Growth potential for species in conjunction with Richard planter form raises some concern with regard to potential sustainability. Small stature would allow for ready replacement.	t	L	C2
1	Oak (Quercus robur)	S/M	G	6.00	2.00	2.50	2.50	2.00	2.50	1	197	2.37	Young and vigorous, planted above car parking entrance structure. Original tiedown hardware is causing strangulation	Remove hardware from lower stem.	L	C2

No.	Species	Age	Con	Ht	СН	Ν	Е	S	W	Stm	Dia	RPA	Structural Condition	PMR	Yrs	Cat
2	Oak (Quercus robur)	S/M	G	5.50	2.00	1.75	1.50	2.00	1.50	1	181	2.18	Slightly misshapen. Supports minor twiggy deadwood suggesting less vigorous status than tree A. Tiedown hardware including cables have caused strangulation and stem cutting near ground level	Remove hardware from lower stem.	L	C2
3	Oak (Quercus robur)	S/M	G	5.50	2.00	2.25	2.50	2.25	1.25	1	210	2.52	Young and vigorous though misshapen and typically unbalanced to east. Vigour is good. Original tiedown hardware is causing strangulation near stem base.	Remove hardware from lower stem.	L	C2
10	Hawthorn (Crataegus monogyna)	М	G/F	4.50	0.00	2.25	2.25	2.25	2.25	1	229	2.75	A broadly young and still vigorous specimen encroached upon at lower levels by extensive Bramble thicket.		L	B2
11	Elder (Sambucus nigra)	E/M	F/P	3.00	0.00	2.00	2.00	2.00	2.00	m/s	175	2.10	Comprising a dominating element of natural thicket redevelopment. Would not typically be regarded as suitable for retention as part of a Development.	Consider early removal.	N/A	U
GW1	Goat Willow <i>(Salix caprea)</i>	S/M	F	5.00	0.50	2.00	2.00	2.00	2.00	m/s	175	2.10	Comprises a natural element of scrub redevelopment.		М	C2
GW2	Goat Willow <i>(Salix caprea)</i>	S/M	F	3.50	0.00	2.00	2.00	2.00	2.00	m/s	143	1.72	Comprises a natural element of scrub redevelopment.		М	C2

No.	Species	Age	Con	Ht	CH	Ν	E	S	W	Stm	Dia	RPA	Structural Condition PMR	Yrs	Cat
WG1	Common Alder (Alnus glutinosa) Red Alder (Alnus rubra) Oak (Quercus robur) Ash (Fraxinus excelsior) Norway Maple (Acer platanoides) Hawthorn (Crataegus monogyna) Wild Cherry (Prunus avium)	S/M	G/F- P	3.50-17.00	0.00-2.00								A small remnant of what appears to have been a larger but recently planted population. Trees narrow arise from heavily disturbed and contaminated ground. Some specimens are dyed others have suffered direct mechanical damage. Tree population constitutes an insignificant proportion of the broader adjoining park population. The loss of these trees will constitute no significant visual loss and many are considered likely to be lost to existing degrees of damage and disturbance. Remove and replace in line with finalised and completed landscape works.	S	C2
WG2	Hazel (Corylus avellana) Hawthorn (Crataegus monogyna) Ash (Fraxinus excelsior) Silver Birch (Betula pendula) Oak (Quercus robur) Hybrid Black Poplar (Populus x Canadensis) Wild Cherry (Prunus avium)	S/M	G/F	4.50-10.00	0.00-2.00								A significant and densely planted corridor of trees. Clear majority of specimens are of good overall condition however, continued growth and coalescence of canopies will result in suppression. Population thinning is advised.	L	B2



Traffic Count Data

MH21009 | Large-scale Residential Development 'Swift Square Apartments' | F01 | July 2023 **rpsgroup.com**







C MapTiler C OpenStreetMap contributors

B

St Mat aret's Rd

IDASO

Survey Name:
Site:
Location:
Date:

029 19025 Northwood 1

St Margaret's Rd 12-Feb-2019

Google

N	/lap data ©2	019 Google								
TIME	A1	A2	A3	B1	B2	B3	B4	C1	C2	C3
07:00	5	25	25	200	120	25	10	5	35	30
07:15	10	25	25	180	130	20	25	10	50	45
07:30	5	25	25	220	200	25	20	5	65	50
07:45	5	35	30	170	160	55	35	15	90	70
08:00	5	40	35	300#	300#	35	50	5	125#	90
08:15	15	35	35	300#	300#	45	15	5	80	55
08:30	5	40	30	300#	300#	40	35	5	85	50
08:45	5	45	30	200	240	40	25	0	125#	70
09:00	5	30	25	300#	300#	30	20	0	125#	100
09:15	0	25	25	180	120	15	15	10	115'#	125#
09:30	0	15	20	170	130	20	30	10	75	50
09:45	0	20	15	180	140	25	20	15	50	40
10:00	15	10	15	150	100	30	20	5	55	35
10:15	15	15	10	75	50	40	50	0	50	30
10:30	5	25	15	100	75	35	40	0	40	35
10:45	5	20	20	90	50	30	30	0	50	30
11:00	5	20	20	100	80	35	50	5	40	30
11:15	10	20	20	30	30	20	45	0	50	25
11:30	15	15	15	45	35	25	35	5	50	40
11:45	20	55	45	120	80	30	40	5	45	35
12:00	5	55	45	110	70	30	30	0	125#	125#
12:15	10	35	40	45	35	25	45	0	125#	70
12:30	15	45	40	50	30	45	50	0	55	40
12:45	10	55	55	45	30	50	65	15	40	30

TIME	A1	A2	A3	B1	B2	B3	B4	C1	C2	C3
13:00	0	20	25	120	70	25	55	0	50	40
13:15	15	25	35	120	80	35	50	0	80	45
13:30	15	40	40	90	45	50	30	0	50	35
13:45	20	60	50	55	40	45	55	15	40	35
14:00	10	40	40	60	40	35	40	0	45	40
14:15	0	35	35	90	50	40	35	5	45	35
14:30	0	20	25	90	90	25	25	0	30	30
14:45	25	25	35	60	40	30	40	0	55	45
15:00	40	25	20	130	70	55	35	0	45	40
15:15	55	40	35	120	80	30	40	0	125#	50
15:30	35	45	40	140	100	25	25	0	55	45
15:45	20	30	35	120	90	40	50	0	70	45
16:00	55	40	45	130	100	20	20	0	65	40
16:15	45	50	45	150	120	35	30	0	125#	55
16:30	50	35	30	100	110	25	25	0	80	40
16:45	60	50	60	130	100	30	30	0	65	60
17:00	0	60	60	90	70	45	30	10	125#	125
17:15	75	50	40	110	90	35	25	15	125#	125
17:30	35	35	40	160	140	25	20	0	125#	125
17:45	35	30	30	95	70	40	30	10	125#	125
18:00	30	40	35	60	45	35	30	0	125#	125
18:15	50	30	30	90	65	40	30	0	55	40
18:30	25	35	40	45	30	30	30	10	60	40
18:45	25	40	30	40	30	25	25	5	40	40

Queue's are measured in meters

Cannot be seen from camera

- + Signifies queue stretches to a minimum length of x and beyond the view of the camera
- # Signifies queue stretches to the next significant junction
- * Indicates an estimated queue length due to obscured vision.









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H/TOT	0 0	0 0	0	0 0	0 2	0 } 0	0 28	7 15	4 (0 2	308 319	9.5 1	1 155	15	2 0	0 1 174	181.1	0 0 2	70 24	5	1 1	301 317	.82 0	0 2	0	0 0		2 2 2	ş.,	0 691	102 3	10 18		172 007 1		147				ing.											in
13:00	0 0	0 0	0	0 0	0	0 2 0	0 83	3 4	4 (0 0	91 9	15 1 1	0 52	4	0 0	0 57	58.2	0 1	19 6	1	0 0 2	57 59	• 2 0	0 1	0	0 0	un fr			0 154	26	7 7								Sunda				und							ini.
13:15	0 0	0 0	0	0 0	0 1	0 0	0 82	2 9	1 0	0 0	92 9	0	0 40	2	0 0	0 42	43	0 0	51 B	1	0 0 1	60 Fee		0 0	0	0 0				3 184	20									1	0 0 197		9 2		135 258.1	5 0	0 0	0 0	0	° :	0
13:30	0 0	0 0	0	0 0		0 1 0	0 69	2 7	1 0	0 0	77 8		0 33	3	0 0	0 36	37.5	0 0	58 2	1	2 0 3	63 67								0 201			11							30	0 0 171	1 29	/ *		210 2243.4	0	0 0	0 0	0	° :	0
13:45	0 0	1 0	0	0 0	. 1		0 76		1		17 . 94		0 16										3							0 201	17	0 9		238 200.2	2 0	40	1 1	0	0 44	43.4	0 1 184	4 33	10 9	7 5 7	244 283.6 5	0	0 0	0 0	0	•	0
H/TOT	0 0	1 0	0	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~		1 2 0	0 310	0 26			347 . 367		0 163	16													mini		<u>.</u>	1 100		9 9		207 234.3	0 0	48	3 1		0 1 52 	in sa	1 0 188	8 25	8 3	2	227 {248.6 }	0	0 0	0 0	0	0	0
14-00	0 0																		12 10			230 5248			0	0 0		in fine	£	3 707	94 2	24 32		871 980.8	2 0	165	6 5	0	0 1 178	181.9	1 1 740	0 109	34 22	15 1	22 { 1036 }	0	0 0	0 0	0	0	0
14.15					11										2 0		47.7	0 0	52 6	1	0 1 5	60 5 64.	5 0	0 0	0	0 0	° [0 1 0	e .	1 161	30	2 7	3 2	204 231.5	2 0	42	3 0	0	0 47	46.9	0 0 197	7 26	4 3	1 1 1	231 250.9	0 0	0 0	0 0	0	0	0
14.15							0 68		0 3		73 76		0 49	0	0 0	0 50	49.2	0 0	52 6	0	0 0 0	58 61	1 3 0	0 0	0	0 0	0	0 0	£ *	0 162	28	9 4	5 2	209 236.9	2 0	34	3 0	0	0 39	38.9	0 0 190	0 28	5 8	3 } ;	234 263.9	0 0	0 0	0 0	0	0	0
14.30	0 0						0 70		0 0	0 0	70 8	52 - 0	0 34	0	0 0	0 34	34 1	0 0	50 6	0	0 1 }	57 { 61	1 2 0	0 0	0	0 0	0	0 2 0	0	1 156	18	6 5	4 1	190 211.9	1 0	39	4 1	0	0 45	46.7	1 0 191	1 20	6 6	3 } ;	227 2 250 2	0 0	0 0	0 0	0	0	0
14:45	0 0	1 0			. i fu	1 3 0	0 55	5 10		0 0	65 7	0 0	0 31	4	1 0	0 36	38.5	0 0	52 3	1	2 1 }	59 64.	6 3 0	0 0	0	0 0	0	0 0	0	1 177	20	5 7	4 2	214 239	0 0	46	2 1	0	0 49	50.5	0 0 199	9 30	7 6	4 } 2	46 276.3	0 0	0 0	0 0	0	0	0
н/тот	0 0	2 0			- inter	2 3 0	1 27	7 29	0 1	1 1	309 325	5.2 2	0 157	5	3 0	0 167	169.4	0 0 2	06 21	2	2 3 }	234 251	1 0	0 0	0	0 0	0	0 : 0	1	3 656	96 2	22 23	16 8	817 919.3	5 0	161	12 2	0	0 180	183	1 0 777	7 104	22 23	11 } 1	138 1041) 0	0 0	0 0	0	0	0
15:00	0 0	0 0	0	0 0 5	0	0	0 68	8 4	0 0	0 0	72 7	-4 0	0 38	8	0 0	0 46	50	0 0	3 10	1	0 0 }	54 } 59.	5 3 0	0 0	0	0 0	0	0 0	0	0 201	23	8 7	6 2	245 275.6	1 0	43	3 0	0	0 47	47.7	1 1 249	9 32	14 5	3] 3	105 336.1	0 0	0 0	0 0	0	0	0
15:15	0 0	0 0	0	0 0 5	0	0 0	0 89	9 11	1 2	2 O	103 111	1.6 0	0 37	6	1 0	0 46	50.5	0 0	56 4	0	0 0 }	60 } 63	2 2 0	0 0	0	0 0	0	0 0	0	1 177	25	3 4	1 2	211 230.6	2 0	33	1 0	0	0 36	34.9	0 1 234	4 25	7 8		276 302.8	0 0	0 0	0 0	0		0 :
15:30	0 0	0 0	0	0 0	0	0	0 81	1 7	0 1	1 0	89 93	.8 0	0 34	2	2 0	0 38	40	0 0	48 3	0	0 0}	51 \$ 52.	5 0	0 0	0	0 0	0	0 : 0	2	0 165	17	4 8	7 2	203 229.3	0 0	36	0 0	0	0 36	36	0 0 240	0 36	7 6	2 2 1	191 322.3	0	0 0	0 0	0	0	0
15:45	0 0	0 0	0	0 0	0 8	0 0	0 61	1 5	1 0	0 0	67 : 7	1 1	0 41	4	2 0	0 48	50.2	2 0	53 4	1	0 2	62 } 64.	9 0	0 0	0	0 0	0	0 0	0	2 181	24	5 7	7 2	226 255.4	2 0	49	4 0	0	0 55	55.4	0 1 253	3 39	3 4	5 2 3	105 335.6	0	0 0	0 0	0		0
H/TOT	0 0	0 0	0	0 0	0	0 0	0 299	9 27	2 3	3 0	331 345	9.4 1	0 150	22	5 0	0 178	190.7	2 0 2	00 21	2	0 2 }	227 238	193 0	0 0	0	0 0	0	0:0	2	3 724	89 2	20 26	21 8	885 990.9	5 0	161	8 0	0	0 1 174	174	1 3 976	6 132	31 23	11 3 1	177 \$ 1297 \$	0	0 0	0 0			~
16:00	0 0	0 0	0	0 0	0 }	0 0	0 88	8 9	1 (0 0	98 10	03 : :	0 46	3	0 0	0 50	50.7	0 0	48 3	2	0 1 }	54 57.	5 0	0 0	0	0 0	0 }	0:0	0	0 188	29	3 1	5 2	226 248.3	3 0	30	2 1	0	0 36	35.1 3	0 2 317	7 36	7 5	man gar	170 399.8	0	0 0	0 0		min	~
16:15	0 0	0 0	0	0 0	0 5	0 0	0 68	9 8	1 0	0 0	78 8	2 2	0 53	6	1 0	0 62	63.9	0 0	9 8	0	0 0	57 5 61	1 3 0	0 0	0	0 0	0	0 0	Ε.	2 214	32	9 6	4 2	268 298.3	1 0	42	2 0	0	0 45	45.2	0 1 332	45			101 431 4		o o				
16:30	0 0	0 0	0	0 0	0	0 0	0 10	9	1 0	0 0		16 1	0 51	:	0 0	0 53	52.7	0 1	45 10	1	0 2	59 65.	0 50	0 0	0	0 0			ł .	2 221	22	4 3		257 277 7	1 0	31		0			0 0 373	1 67	1 4		1						
16:45	0 0	0 0	0	0 0	0 2	0 0	0 67	7 6	0 1	1 0	74 78	1.3 1	1 53	9	0 0	0 64	67.1	0 1	47 8	1	0 0	57 60.		0 0	0	0 0		0 0	ł .	2 191	21	2 2	2	226 246 6	0 0	34		0			0 1 000							0 0			
H/TOT	0 0	0 0	0	0 0 2	0 2	0 0	0 324	4 33	3 3	1 0	361 380	0.3 5	1 203	19	1 0	0 229	234.4	0 2 1	89 29	4	······	227 245	32 0	0 0	0	0 0			£	6 814	104	18 17																0 0		minie	
17:00	0 0	0 0	0	0 0	0	0 1	0 11	3 16	2 0	0 0	132 140	0.2 0	2 43	1	1 0	0 47	46.8	0 0	11 10	1	0 0 2	42 47	5 2 0	0 0	0	0 0			£	2 228	29			271 207 3		12				40.3	135		20 21		1730 3		- 0	0 0		minie	in:
17:15	0 0	0 0	0	0 0		0 0	0 71	6	2 0		79 8		0 46	2	1 0	0 51	51.3	0 0	16. 7										E .		20					34	5 0	0		40.3	0 2 394	4 49	2 5	1	154 2480.8	0	0 0	0 0	0	•	0
17:30	0 0	0 0	0	0 0		0 0	0 57	7 7	1 1	0 0	65 . 6	4	1 14	5	0 0		42.7	0 0												- 227	20			200 . 287.8	0 0	31	: 0	0	0 32	32.5	2 2 394	35	4 6		48 477.1	0	0 0	0 0	0	0	0
17:45	0 0	0 0	0	0 0		0 0	0 41		2	0 0	50	15 0	0 10	2	0 0			0 0		,					0	0 0				- 250	25	3 2		310.2	1 0	42	1 0	0	44	43.7	1 3 406	5 38	2 6	7	495.2	0	0 0	0 0	0	0	0
H/TOT	0 0			0 0			0	2 14			126	67					to and				·····		3				····		ļ	2 247	28	* 6	1 2	291 315.8	2 0	49	3 1	0	0 55	55.4	1 2 366	6 24	3 5	4.1.4	427	0	0 0	0 0	0	0	0
18:00													3 102			0 185	162.8	0 0 1	w 26			-19 23	·		0	0 0		0 0	į , , ,	12 952	102 2	20 17	16 11	122 1212	7 0	154	10 1	0	0 172	171.9	2 9 1564	4 146	11 22	16 1	770 1886 }	0	0 0	0 0	0	0	0
10.15	0 0						0 04						0 41	3	0 0	46	43.9	0 0	1	1		45 5 46		0 0	0	0 0	0	0 : 0	0	0 197	18	5 6	4 2	230 253.3	2 0	41	1 0	0	0 1 44	42.9	0 0 319	9 11	5 6	2 3 3	43 360.8	0	0 0	0 0	0	0	0
10.12	~ 0		0				0 67				09 7		2 33	3	0 0	0 39	38.5	0 0	40 4	0	0 0	52 } 54		0 1	0	0 0	0	1 1 1	0	1 199	12	2 4	1 2	219 231.6	4 0	44	2 0	0	0 50	47.8	2 310	0 21	6 2	5 2 3	46 365.9	0	0 0	0 0	0	0	0
18:30	0 0	0 0	0				0 55		0 0	0	50 59		0 46	1	0 0	0 48	47.7	0 0	49 1	0	0 0	50 } 50.	5 0	0 0	0	0 0	0	0 0	1.	4 183	12	4 3	3 2	210 221.7	1 1	33	1 0	0	0 36	35.1	0 2 205	5 13	2 4	2 2 2	28 241.5	0	0 0	0 0	0	0	0
18:45	0 0	0 0	0	0 0			1 58		0 0	0 1	63 : 64		0 34	3	0 0	0 37	38.5	0 0	50 5	0	0 0 }	55 } 57.	5 0	0 0	0	0 0	0 }	0 : 0	0	0 174	14	2 1	6 1	197 212.3	0 1	40	2 0	0	0 43	43.4	0 1 234	4 10	3 4	6 2 2	158 275.1	0	0 0	0 0	0	0	0
н/тот	0 0	0 0	0	0 0 3		0 0	1 24	4 14	1 0	0 1	261 268	8.9 4	2 154	10	0 0	0 170	170.6	0 0 1	90 11	1	0 0 }	202 20	8 3 0	0 1	0	0 0	0	1 1	1	5 753	56 1	13 14	14 8	856 918.9	7 2	158	6 0	0	0 173	169.2	0 5 1066	8 55	16 16	15 1	175 1243	0	0 0	0 0	0	0	0
12 TOT	0 0	4 0	0	0 0 5	* }	• . •	6 263	30 260	51 1	12 8	2971 : 31	43 ; 41	7 1720	166	29 2	1 1966	2030	2 4 2	499 251	36	12 20 }	2824 295	99 0	0 4	0	0 0	0	4 4	13 1	54 10922	1344 3	05 339	168 13	3145 14535	48 5	1680	114 28	1	3 1879	1913 1	2 35 9903	1 1282	328 271	158 11	987 13272	0	0 0	0 0	0	0	0

Homebase - C



Survey Name: Site: Location: Date:

2 R108 / Northwood Ave 12-Feb-2019

029 19025 Northwood

Google

	Map data ©	2019 Google								
TIME	A1	A2	A3	B1	B2	B3	B4	C1	C2	C3
07:00	15	20	25	10	30	15	40	30	50	50
07:15	20	60#	40	5	20	0	25	30	50	40
07:30	15	45	25	0	20	15	30	40	40	60
07:45	20	15	30	30	10	0	20	30	125#	70
08:00	15	60#	40	10	50	10	20	20	80	125#
08:15	15	60#	40	25	20	10	25	30	125#	125#
08:30	10	60#	40	5	30	5	80	40	125#	60
08:45	15	30	20	15	30	15	80	60	125#	50
09:00	10	60#	40	10	35	30	50	20	30	20
09:15	10	50	30	15	30	15	50	40	100	30
09:30	20	60#	40	15	35	5	30	20	50	40
09:45	20	60#	30	15	10	0	50	20	30	40
10:00	15	60#	30	5	20	10	20	25	25	30
10:15	20	60#	35	5	15	5	25	20	30	40
10:30	15	60#	25	0	15	5	20	15	20	25
10:45	15	30	30	10	15	5	10	20	25	30
11:00	10	40	35	15	20	5	20	30	15	10
11:15	25	40	35	10	20	5	15	15	20	20
11:30	15	40	20	15	20	10	25	10	25	30
11:45	15	30	20	10	20	15	20	15	20	20
12:00	20	30	20	15	20	10	35	10	15	20
12:15	20	50	15	0	20	25	20	15	30	20
12:30	10	40	20	10	20	10	30	20	20	25
12:45	25	50	30	10	20	10	25	30	15	30

TIME	A1	A2	A3	B1	B2	B3	B4	C1	C2	C3
13:00	25	30	40	5	30	20	45	30	20	30
13:15	20	50	30	20	25	20	20	15	20	15
13:30	25	60#	30	15	35	20	30	15	30	25
13:45	30	60#	20	15	30	25	110	25	20	20
14:00	50	60#	30	20	30	10	30	10	30	20
14:15	20	60#	40	10	40	5	30	15	30	20
14:30	30	60#	40	15	30	25	30	15	20	15
14:45	30	60#	30	10	20	5	25	15	30	125#
15:00	20	60#	25	10	25	20	30	25	50	30
15:15	40	60#	25	0	20	10	30	10	40	30
15:30	30	60#	40	10	30	15	35	15	25	15
15:45	15	60#	45	5	40	10	30	10	20	15
16:00	50	60#	35	15	110	15	30	5	20	25
16:15	30	60#	30	5	20	20	40	15	20	15
16:30	20	50	40	5	110	15	30	15	30	20
16:45	20	60#	40	15	115	15	35	20	25	35
17:00	50	60#	40	5	150	30	40	15	20	15
17:15	60#	60#	40	15	165	130	30	10	15	10
17:30	60#	60#	40	10	130	20	40	15	35	25
17:45	40	60#	30	15	70	20	40	15	10	15
18:00	30	60#	20	10	100	20	30	15	40	20
18:15	20	60#	40	5	120	15	35	10	20	15
18:30	20	50	30	5	30	15	10	10	15	10
18:45	20	50	30	15	20	15	15	5	15	35

Queue's are measured in meters

Cannot be seen from camera

- + Signifies queue stretches to a minimum length of x and beyond the view of the camera
- # Signifies queue stretches to the next significant junction
- * Indicates an estimated queue length due to obscured vision.







		A => A	}		A => 8		A => C		5 => A	3	8 => 8		-	8 => C	1 1	C => A		C => 8		C => C		
TIME	P/C M/C	CAR LGV OGV1 OGV2	PSV TOT	PCU P	C M/C CAR LGV OGV1 OGV2	2 PSV TOT P	CU P/C M/C CAR LOV OGVI DOV	2 PSV TOT PCU	P/C M/C CAR LGV OGV1 OGV2 PS	TOT PCU	P/C H/C CAR LGV OGV1 OGV2 PS	TOT PC	P/C H/C CAR	LGV OGV1 OGV2 PS	V TOT PCU	P/C M/C CAR LGV OGV1 OGV2	PSV TOT PCU P/	C M/C CAR LGV OGV1 OGV2 P	SV TOT PCU P	C M/C CAR LGV OG	V1 OGV2 PSV	TOT PCU
07:00	0 0	0 0 0 0	0 0	0	0 0 17 3 0 0	0 20 21	1.5 0 0 27 4 3 3	0 37 44.4	0 0 9 2 1 0 0	12 13.5	S 0 0 0 1 0 0 0	1 1.5	0 0 72	19 3 2 2	98 113.6	0 0 66 22 1 10	0 99 123.5 0	0 218 24 5 1	252 271.8	0 0 0 0	0 0	0 0
07:15	0 0	0 0 0 0	0 0	0	0 0 29 4 0 0	0 33 3	35 0 0 22 4 1 5	0 32 41	1 0 13 3 0 0 0	17 17.7	7 0 0 1 1 0 0 0	2 2.5	1 1 95	20 0 0 1	118 127.6	0 1 74 25 6 8	0 114 139.3 0	0 0 209 46 8 4	270 305.2	0 0 0 0	0 0	0 0
07:30	0 0	0 0 0 0	0 0		0 0 24 7 2 0	0 33 37	7.5 0 0 52 7 8 10	0 77 97.5	2 0 18 1 0 0 0	21 19.9	0 0 3 0 0 0 0	1 1 3	2 2 132	12 5 0 3	156 164.7	0 0 122 18 1 9	1 151 173.2 0	0 0 241 40 8 2	294 323.6	0 0 0 0 0	0 0	0 0
07:45	0 0	0 0 0 0	0 } 0	0 0	0 1 20 3 0 0	0 24 24	4.9 0 0 47 4 1 0	1 53 56.5	1 0 9 1 1 0 0	12 12.2			0 6 148	13 4 2 3	176 186.5	0 1 132 6 1 3	0 143 149.8 1	4 337 50 7 2	405 \$436.9 \$	0 0 0 0 0	0 0	
н/тот	0 0	0 0 0 0	· · · · ·	0	0 1 90 17 2 0	0 110 11	8.9 0 0 148 19 13 18	1 199 239.4	4 0 49 7 2 0 0	62 63.3	1 0 0 5 2 0 0 0		3 9 447	64 12 4 9	548 592.4	0 2 394 71 9 30	1 507 585.85 1	4 1005 160 28 9 1	4 1221 1338	0 0 0 0 0		
08:00	0 0	0 0 0 0	0 0	0	0 1 25 7 0 0	0 33 3	5.9 0 0 49 9 2 3	0 63 72.4	0 0 18 2 0 0 0	20 21			0 2 172	21 1 3 1	200 214.7	1 1 157 9 4 1	0 173 179.4 0	3 325 35 4 1	3/1 393	0 0 1 0 0	0 0	
08:15	0 0	0 0 0 0	0 5 0		0 0 38 6 0 0	0 44		0 57 67.7		19 4.5				10 4 7 7	103 107 3		0 211 227 5 0	2 203 22 2 1	111 120.1		0 0	
08:30	0 0	0 0 0 0	0		0 2 36 3 3 0	0 44 4	3.8.0 0 46 5 5 4	0 00 102		1 20 1 20.5			0 0 155	18 1 1 4	183 201.4		0 221 237 0	2 266 24 3 1	200 315.6		0 0	
08:45	0 0				0 0 31 3 0 1	0 1 156 146	4.5 2 0 171 23 16 15	0 227 2764 4		100 2108.1		10 10	1 2 630	79 13 7 9	741 803.1	2 3 706 43 13 22	0 789 842.2 0	8 1199 102 19 3	4 1345 1419	0 0 1 0 0	0 0	
09-00					0 0 27 7 0 1	0 35 3	9.8 0 0 40 14 6 4	0 64 79.2	0 0 27 2 0 0 0	29 30	2 0 0 2 0 0 0 0	2 2	0 1 151	17 9 0 4	182 198.4	0 0 126 13 0 4	0 3 143 3 154.7 3 0	0 253 18 6 4	285 306.23	0 0 0 0	0 0	0 0
09:15	0 0	0 0 0 0			1 0 32 0 1 0	0 34 33	3.7 0 0 36 13 6 3	1 59 73.4	0 0 33 6 0 0 0	39 42	0 0 4 1 0 0 0	5 5.5	0 1 158	18 5 1 7	190 209.2	1 1 119 14 8 8	1 152 173 0	1 226 23 1 3	257 275.3		0 0	0 0
09:30	0 0	0 0 0 0	0 0		0 1 26 6 2 0	0 35 36	8.4 1 0 56 6 3 4	0 70 78.9	0 0 13 1 2 0 0	16 17.5	sto o 2 o o o o	2 2 2	0 0 129	15 5 1 1	151 163.3	2 1 92 10 1 9	0 115 130 1	1 244 27 7 3	284 304.5	0 0 0 0	0 0	0 0
09:45	0 0	0 0 0 0	0 0		0 1 21 7 0 0	0 29 31	1.9 0 0 40 7 8 6	0 61 76.3	1 0 33 4 0 0 0	38 39.2	2 0 0 3 1 0 0 0	4 45	3 0 96	23 3 5 7	137 161.1	0 0 84 16 3 9	0 112 133.2 0	1 191 32 7 2	237 262.5		0 0	0 0
н/тот	0 0	0 0 0 0	0 0	0	1 2 106 20 3 1	0 133 14	3.8 1 0 172 40 23 17	1 254 307.8	1 0 106 13 2 0 0	122 128.1	7 0 0 11 2 0 0 0	13 14	3 2 534	73 22 7 19	660 732	3 2 421 53 12 30	1 522 590.9 1	3 914 100 21 12 1	2 1063 1149	0 0 0 0	0 0	0 0
10:00	0 0	0 0 0 0	0 0	0	0 0 21 3 0 0	0 24 2	5.5 0 0 44 4 3 8	0 59 72.9	0 0 16 2 1 0 0	19 20.5	5 0020000	2 2	2 0 102	26 4 3 4	141 162.3	1 0 65 2 2 4	0 74 80.4 0	0 147 19 6 1	176 192.8	0 0 0 0	0 0	0 0
10:15	0 0	0 0 0 0	0 0	0	0 0 25 5 1 0	0 31 1	34 0 0 49 7 4 6	0 66 79.3	2 0 15 3 1 0 0	21 21.4		2 2	1 2 102	12 10 3 10	140 162.9	0 0 80 8 2 6	0 96 108.8 0	0 0 142 22 3 1	171 187.8		0 0	0 0
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11:00	0 0	0 0 0 0	0 { 0	0	0 0 30 2 0 0	0 32 3	33 0 0 50 5 4 2	0 61 68.1	0 0 11 1 0 0 0	12 12.5	5 0 0 2 0 0 0 0	2 2 2	0 0 125	23 6 3 3	160 181.4	0 0 61 8 2 11	0 82 101.3 0	0 0 117 19 4 0	144 159.5	0 0 0 0	0 0	0 0
11:15	0 0	0 0 0 0	0 0	0	0 0 32 5 1 0	0 38	41 0 0 45 7 5 10	0 67 86	0 0 15 2 0 0 0	17 18	0 0 1 0 0 0 0	1 1	0 0 130	14 6 2 2	154 168.6	1 0 68 5 0 7	0 81 91.8 1	0 123 17 7 4	154 172.4	0 0 0 0	0 0	0 0
11:30	0 0	0 0 0 0	0		0 0 26 2 0 0	0 28	29 1 0 36 5 2 2	0 46 51.3	0 0 17 3 0 0 0	20 21.5	5 0 0 1 0 0 0 0	1 1 1	0 0 148	23 8 2 4	185 207.1	0 0 43 11 4 5	0 63 77 0	0 0 131 16 8 3	2 160 177.9	0 0 0 0 0	0 0	0 0
11:45	0 0	0 0 0 0	0 0	0	2 0 35 6 0 0	0 43 4	4.4 0 0 43 9 3 5	0 60 72.5	0 0 17 3 0 0 0	20 21.5	5 0 0 1 0 0 0 0		0 1 121	20 6 2 3	153 : 171	0 0 67 12 5 10	0 5 94 5115.55 3	1 137 27 8 2	181 201.1	0 0 0 0 0	0 0	0 0
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12:15	0 0	0 0 0 0	0 0 0		0 0 30 4 2 1	0 37 4	1.3 1 0 54 5 3 4	0 6/ 75.4		15 13.3			1 0 138	29 3 1 5	177 1108 5	0 0 66 5 2 6	0 60 80.3	0 151 21 9 2	185 204.6		0 0	
12:30	0 0	0 0 0 0			1 0 34 4 1 0	0 40 40	17 0 1 67 5 2 1	0 78 84.8	0 1 25 2 1 1 0	30 322		7 6.9	0 0 129	17 5 3 0	154 168.9	0 0 73 13 2 6	0 94 109.3 0	0 132 27 5 1	167 186.3		0 0	0 0
H/TOT					1 0 127 16 4 1	0 149 15	59.5 3 1 236 27 14 10	0 291 321.5	1 1 80 8 1 2 0	93 98.7	7 0 1 14 2 0 0 0	17 17.	1 2 544	80 18 9 8	662 728.7	1 0 273 32 7 24	0 337 386.9 0	0 1 559 83 21 14 1	1 689 769.6	0 0 2 0 0	0 0	2 2
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13:15	0 0	0 0 0 0	0 0		1 0 51 2 0 0	0 54 54	4.2 0 0 64 4 4 7	0 79 92.1	0 1 18 3 0 0 0	22 22.9	9 0 2 1 0 0 0	3 3.5	1 0 144	20 6 3 2	176 194.1	0 1 81 13 1 5	0 101 113.9 0	0 1 147 18 1 2	172 186.5		0 0	0 0
13:30	0 0	0 0 0 0	0 0		1 1 54 4 0 0	1 61 6	2.6 1 0 66 9 5 5	0 86 98.7	0 0 27 2 0 0 0	29 30		6 6	0 1 161	26 6 3 6	203 228.3	0 0 77 6 4 7	1 95 110.1 0	0 0 154 15 2 2	177 192.1		0 0 0	0 0
13:45	0 0	0 0 0 0	0 0		1 0 44 5 0 0	0 50 5	1.7 0 0 79 8 2 2	0 91 98.6	1 1 38 7 0 0 0	47 49.1	1 0 0 2 1 0 0 0	3 3.5	0 0 157	20 6 0 2	185 200	0 0 72 12 5 7	0 96 113.6 0	0 1 134 19 6 2	163 178.5	0 0 0 0	0 0	0 0
H/TOT	0 0	0 0 0 0	0 0	0	4 1 197 12 2 0	1 217 22	21.2 1 0 292 31 14 16	1 355 398.5	1 2 109 16 0 0 0	128 134	4 0 0 14 2 0 0 0	16 17	1 1 627	80 25 6 14	754 826.9	0 1 317 36 14 24	1 393 449.6 0	0 2 561 73 12 8 1	0 666 727.7	0 0 0 0	0 0	0 0
14:00	0 0	0 0 0 0	0 0	0	0 0 43 7 1 0	0 51	55 0 0 58 7 2 2	0 69 76.1	0 0 19 1 0 0 0	20 20.5	s 0 0 4 0 0 0 0	4 4	0 0 183	22 2 1 1	209 223.3	0 0 55 4 2 7	0 68 80.1 1	1 1 149 22 2 0	178 191.6	0 0 0 0	0 0 0	0 0
14:15	0 0	0 0 0 0	0 0		2 0 37 2 1 0	0 42 4	1.9 0 0 57 11 2 6	0 76 90.3	0 0 20 2 0 0 0	22 23	0 0 2 0 0 0 0	2 2 2	0 0 160	20 5 3 3	191 210.4	1 0 67 10 2 2	0 82 89.8 1	1 1 146 19 7 2	5 181 200.2	0 0 0 0	0 0 0	0 0
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15:15	0 0	0 0 0 0			1 0 48 0 0 0	0 43	45 0 0 72 15 1 4	1 91 107.3		11 12			0 0 193	23 5 2 2	225 243.6	1 0 56 6 3 5	0 71 81.2 0	0 0 142 15 3 3	7 170 189.93	0 0 0 0 0	0 0 0	0 0
15:45	0 0	0 0 0 0	0 0		1 0 44 13 0 0	0 58 6	3.7 2 0 69 15 2 2	0 90 99.5	0 0 21 2 0 0 0	23 24	0 0 5 0 1 0 0	6 6.5	0 1 245	36 5 1 5	293 319.2	0 0 68 11 5 3	0 87 98.9 0	0 2 163 18 2 4	7 196 217	0 0 0 0	0 0 0	0 0
H/TOT		0 0 0 0		0	3 0 168 21 1 1	0 194 20	03.9 4 0 287 43 9 11	1 359 402.3	0 0 97 9 3 0 0	109 115	5 0 0 14 0 1 0 0	15 15.	0 3 843	105 25 7 11	994 1077	1 0 268 38 13 16	0 336 381.53 0	0 3 614 74 11 10	1 733 807.7	0 0 0 0	0 0	0 0
16:00	0 0	0 0 0 0		101	1 0 41 10 0 0	0 52 5	6.2 3 0 90 15 4 4	0 116 128.3	0 1 19 3 0 0 0	23 23.5	9 0 0 7 0 0 0	7 7	0 2 246	20 1 2 4	275 290.9	0 0 71 11 0 2	0 84 92.1 0	0 0 151 21 3 0	5 180 197	0 0 0 0 0	0 0	0 0
16:15	0 0	0 0 0 0	0 0	0	1 0 41 7 0 1	0 50	54 1 0 82 13 1 2	0 99 107.8	0 0 29 2 1 0 0	32 33.5	5 0 0 1 0 0 0 0	1	0 1 307	35 7 3 3	356 383.3	0 0 75 6 5 5	0 91 103 1	1 2 188 33 4 0	232 252.5	0 0 0 0	0 0	0 0
16:30	0 0	0 0 0 0	0 0	0	0 0 39 3 1 0	0 43	45 0 0 102 7 1 2	0 112 118.6	0 0 15 5 0 1 0	21 24.8	s { 0 0 4 0 0 0 0	4 4	0 0 283	49 3 3 1	339 369.9	1 1 85 6 3 3	0 99 106 0	0 1 187 18 0 0	5 211 224.4	0 0 0 0	0 0	0 0
16:45	0 0	0 0 0 0	0 0	0	0 0 46 4 0 0	0 50	52 0 1 99 7 1 4	0 112 120.6	0 0 16 3 0 0 0	19 20.5	s 0 0 3 0 0 0 0	1 1 1 3	0 0 284	41 7 1 5	338 368.3	0 1 83 12 1 7	0 104 119 1	1 0 170 20 1 1	2 195 208	0 0 0 0	0 0 0	0 0
H/TOT	0 0	0 0 0 0	0 0	0	2 0 167 24 1 1	0 195 20	07.2 4 1 373 42 7 12	2 0 439 475.3	0 1 79 13 1 1 0	95 102	7 0 0 15 0 0 0 0	15 11	0 3 1120	145 18 9 13	1308 1412	1 2 314 35 9 17	0 378 420.1 2	2 3 696 92 8 1	6 818 881.9	0 0 0 0	0 0 0	0 0
17:00	0 0	0 0 0 0	0 0	0	0 0 70 5 0 0	0 75 7	77.5 1 1 88 9 2 6	0 107 118.5	0 0 13 1 0 1 0	15 16.8	8 0 0 1 0 0 0 0	1 1	2 2 343	36 1 0 1	385 401.7	1 1 93 4 1 2	0 102 105.7 0	0 2 167 27 4 1	5 206 226.6	0 0 0 0	0 0 0	0 0
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17:45	0 0	0 0 0 0	0 0	0	1 1 45 5 0 0	0 52 5	53.1 1 0 95 9 1 4	0 110 119.4	0 0 17 1 0 0 0	18 18.5	3 50031000	4	2 1 326	19 2 1 3	354 366.6	1 0 90 12 3 5	0 111 124.2	1 2 199 14 3 1	223 233.8		0 0	
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18:00	0 0	0 0 0 0	0 0		1 0 59 1 0 1	0 62	63 1 0 95 2 3 5	0 100 114.		1/ 16.5			1 1 260	19 4 1 4	284 300 4		0 73 80.6	0 1 175 10 2 0	190 197.4	0 0 0 0		
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18:30	0 0	0 0 0 0	0		0 0 33 1 0 0	0 34 3	14.5 1 1 61 4 0 1	0 70 74 5	0 0 20 3 0 0	23 24.9	5 0 0 2 1 0 0 0	3 3	0 0 203	12 0 1 6	222 235 3	3 0 0 55 1 1 1	0 58 60.3	0 0 155 13 2 0	6 176 189.5	0 0 0 0	0 0 0	0 0
H/TOT	0 0	0 0 0 0	0 0	0	5 0 166 9 0 1	0 181 1	82.8 6 3 317 18 5 1	0 362 383.4	0 2 66 6 0 0 0	74 75.8	8 0 0 13 1 0 0 0	14 14.	2 4 878	53 6 4 1	962 1008	2 3 253 16 7 14	0 295 321.3 3	3 2 646 44 9 1	5 720 759.2	0 0 2 0	0 0 0	2 2
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Survey Name:
Site:
Location:
Date:

029 19025 Northwood 3 Northwood Ave 12-Feb-2019

1	Map data ©	2019 Google										1	1			1	
TIME	A1	A2	B1	B2	C1	D1	D2	D3	TIME	A1	A2	B1	B2	C1	D1	D2	D3
07:00	0	10	40	60	5	50	30	10	13:00	0	15	40	40	5	60#	50	10
07:15	0	25	75	75	5	40	40	10	13:15	0	20	30	55	10	50	50	10
07:30	10	15	60	75	10	60#	60#	10	13:30	10	25	35	75	5	40	50	20
07:45	15	15	20	30	5	60#	60#	5	13:45	5	25	40	75	10	60#	60#	15
08:00	15	20	30	50	5	40	60#	5	14:00	10	30	40	60	10	60#	50	15
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08:30	10	20	20	20	15	60#	60#	5	14:30	0	20	70	30	10	60#	60#	5
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09:00	0	30	20	70	10	60#	60#	10	15:00	5	25	30	40	5	30	50	5
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10:00	5	20	15	30	5	50	60#	10	16:00	0	30	40	120#	25	30	40	5
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10:30	0	15	30	55	15	25	35	0	16:30	5	15	30	70	5	40	30	10
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11:00	20	20	20	60	5	60#	60#	10	17:00	5	45	50	120#	5	40	50	10
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#### Queue's are measured in meters

Cannot be seen from camera

- + Signifies queue stretches to a minimum length of x and beyond the view of the camera
- # Signifies queue stretches to the next significant junction
- * Indicates an estimated queue length due to obscured vision.

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Survey Name:
Site:
Location:
Date:

029 19025 Northwood 4 Northwood Ave 12-Feb-2019

#### Google

#### Regus - Dublin Santry O Map data ©2019 Google

TIME	A1	B1	B2	C1	C2
07:00	5	10	0	5	0
07:15	10	5	5	20	15
07:30	5	15	10	15	25
07:45	10	10	0	10	15
08:00	10	10	10	5	25
08:15	10	5	5	15	75
08:30	20	5	10	35	95
08:45	25	5	10	30	80
09:00	15	10	10	25	70
09:15	20	10	5	35	50
09:30	15	10	10	20	15
09:45	10	10	10	25	30
10:00	15	5	5	15	20
10:15	15	5	15	10	20
10:30	10	10	10	15	20
10:45	15	10	10	10	20
11:00	30	10	10	10	15
11:15	20	5	10	5	10
11:30	20	15	5	10	15
11:45	15	10	15	15	10
12:00	20	10	5	15	20
12:15	15	10	10	20	30
12:30	15	15	10	15	10
12:45	20	15	15	20	25

TIME	A1	B1	B2	C1	C2
13:00	45	10	15	50	85
13:15	45	15	10	30	75
13:30	20	15	15	20	45
13:45	30	10	15	20	30
14:00	35	15	5	10	20
14:15	25	10	5	15	20
14:30	10	10	15	15	15
14:45	20	10	15	25	10
15:00	20	15	15	20	10
15:15	20	15	15	15	10
15:30	25	20	10	10	15
15:45	25	15	10	30	20
16:00	30	10	15	15	40
16:15	15	15	15	20	15
16:30	30	10	15	10	10
16:45	30	35	30	15	40
17:00	45	40	70	20	30
17:15	45	20	65	10	15
17:30	45	45	85	20	20
17:45	30	50	30	10	15
18:00	15	20	15	15	15
18:15	20	20	10	10	15
18:30	20	10	10	15	25
18:45	15	15	10	10	15

Queue's are measured in meters

Cannot be seen from camera

- + Signifies queue stretches to a minimum length of x and beyond the view of the camera
- # Signifies queue stretches to the next significant junction
- * Indicates an estimated queue length due to obscured vision.

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	P/C M/			0	0 0	0 0	0 0	0 0	0	0 0	0 0	0	0	0 0	0 0	0	0	0 0	0 0	0 0	0	0 0	0 0	0	0 0	0 -			0 0	-	0 0	0 0	0	0 0	0 0
	PCU	15	20.5	292	4 16	1 24.5	25.5	36.5	FR O	127.3 7.1E	0 415 11	2.00	42.5	# R	5 37	92 0	2 2	8 176	4 5 F	12.4	234.3	6 48 2 6 48 2	2 63.5	07 216	3 3	12 52	12 220.5	2 53.5	\$ 0	06 215.5	58.5 65.6	1 412	187.2	38.5	37.5
	PSV T0	0 0			0 0	0 2	0 2		0	. 0	4 X	0	-	0 0	0	0	0 0	0 0	0 0	0 0	0 2	0 0	0 0	0	0 0	0 0	0	0 0	0 0	0	0 0	0 0	0	0 0	0 0
	1 06V2	0 0	0 0 0	0	0 0	0 0	0 0	0 0	-	. 0	0 0	0	0	0 0	0 0	0	0 0	0	0 0	0 0	0	0 0	0 0	0	0 0	0 0	0	0 0	0 0	0	0 0	0 0	0	0 0	0 0
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029 19025 Northwood 5 Northwood Ave 12-Feb-2019

Google

TIME	Δ1	Δ2	B1	R2	C1	C2	D1	D2
07:00	5	0	5	0	5	5	5	5
07.15	10	0	5	0	5	5	5	5
07:15	10	0	0	0	5	10	10	10
07:30	10	5	5	5	10	10	10	15
07:45	5	0	0	5	5	10	15	20
08:00	10	0	0	5	10	5	10	15
08:15	10	0	0	0	10	10	15	25
08:30	5	0	5	0	20	0	10	15
08:45	5	0	10	5	10	10	15	15
09:00	5	10	5	5	5	10	10	20
09:15	5	10	0	5	5	15	15	30
09:30	0	5	5	10	5	10	10	5
09:45	10	5	5	5	5	5	15	5
10:00	10	5	5	5	5	5	10	5
10:15	5	0	10	5	5	5	10	5
10:30	5	0	10	5	5	10	10	5
10:45	5	0	10	0	5	10	5	10
11:00	10	5	5	0	5	5	5	0
11:15	10	5	10	5	10	0	15	0
11:30	5	0	0	0	15	10	15	5
11:45	5	0	15	10	5	10	5	5
12:00	5	5	5	10	5	5	5	5
12:15	5	5	5	5	10	5	0	0
12:30	5	5	5	10	5	10	5	10
12:45	0	15	5	10	20	5	10	15

TIME	A1	A2	B1	B2	C1	C2	D1	D2
13:00	5	15	0	10	10	10	15	10
13:15	10	0	10	0	10	20	5	15
13:30	10	5	5	5	10	10	5	15
13:45	5	5	0	0	10	5	10	15
14:00	5	0	5	10	15	15	15	5
14:15	5	10	5	5	5	0	10	5
14:30	5	5	10	0	10	5	5	10
14:45	5	5	5	0	10	10	10	20
15:00	5	5	5	15	5	10	5	15
15:15	5	10	10	5	10	10	5	10
15:30	10	5	0	0	10	5	10	5
15:45	10	0	10	10	5	5	5	10
16:00	5	5	0	5	5	5	5	5
16:15	10	5	5	5	10	10	20	10
16:30	10	10	0	20	10	15	10	25
16:45	10	15	5	15	5	15	20	15
17:00	10	10	15	10	10	10	10	25
17:15	5	10	15	15	10	25	10	10
17:30	15	10	5	25	10	15	15	20
17:45	5	10	5	10	15	20	5	10
18:00	15	10	10	5	5	10	10	45
18:15	5	5	5	15	15	20	15	10
18:30	10	5	0	10	10	10	10	10
18:45	10	5	10	5	5	5	5	15

Queue's are measured in meters

Cannot be seen from camera

- + Signifies queue stretches to a minimum length of x and beyond the view of the camera
- # Signifies queue stretches to the next significant junction
- * Indicates an estimated queue length due to obscured vision.

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Survey Name:
Site:
Location:
Date:

029 19025 Northwood 6 Forestwood Ave / Santry Ave 12-Feb-2019

N	/lap data ©2	019 Google				
TIME	A1	A2	B1	B2	C1	C2
07:00	10	5	15	5	10	15
07:15	10	10	15	10	10	20
07:30	15	20	30	15	10	30
07:45	15	20	30	10	20	35
08:00	25	20	30	30	5	50
08:15	10	20	40	25	10	60
08:30	45	10	30	25	10	130
08:45	25	10	25	10	30	130
09:00	20	15	40	30	55	120
09:15	15	10	30	20	15	60
09:30	10	10	35	10	10	55
09:45	15	5	55	20	10	50
10:00	10	5	40	5	10	60
10:15	20	5	20	15	15	30
10:30	25	10	30	15	15	40
10:45	15	30	40	10	5	50
11:00	15	5	30	10	5	35
11:15	10	10	20	15	5	30
11:30	15	10	30	15	5	40
11:45	15	10	50	15	5	40
12:00	20	5	30	15	5	60
12:15	20	15	10	5	10	40
12:30	20	15	30	15	5	35
12:45	15	5	50	15	20	120

	TIME	A1	A2	B1	B2	C1	C2
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Ī	14:45	10	15	30	20	15	65
	15:00	15	10	35	30	5	100
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	17:15	40	40	110	45	15	100
	17:30	30	60	120+	30	10	60
	17:45	40	30	90	30	20	100
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	18:30	25	15	45	35	10	55
Ī	18:45	15	20	15	20	10	50

Queue's are measured in meters

Cannot be seen from camera

- Signifies queue stretches to a minimum length of x and beyond the view of the camera +
- Signifies queue stretches to the next significant junction #
- Indicates an estimated queue length due to obscured vision. *





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Survey Name: Site: Location: Date: 029 19025 Northwood 7 Northwood Ave / Swords Rd 12-Feb-2019

TIME	A1	A2	B1	B2	B3	C1	C2
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07:30	20	45	45	150	20	35	100
07:45	45	50	40	70	50	30	110
08:00	35	40	30	130	40	45	120
08:15	55	45	50	180+	30	35	70
08:30	60	55	30	80	50	50	200+
08:45	85	50	20	70	45	40	200+
09:00	40	30	15	150	30	60	120
09:15	60	55	20	100	25	50	200+
09:30	50	30	15	65	20	40	60
09:45	30	25	15	70	20	30	110
10:00	30	25	30	55	15	45	60
10:15	35	30	15	50	25	40	80
10:30	30	35	25	130	15	25	40
10:45	30	50	15	60	10	20	50
11:00	20	35	20	55	25	20	45
11:15	30	40	20	100	30	45	70
11:30	50	35	15	70	15	30	100
11:45	35	40	20	80	20	25	80
12:00	40	25	10	80	30	20	50
12:15	30	50	20	90	20	30	100
12:30	30	40	30	180+	50	30	60
12:45	25	30	30	180+	40	30	110

							-
TIME	A1	A2	B1	B2	B3	C1	C2
13:00	30	30	30	180+	60	30	105
13:15	30	50	20	135	20	50	80
13:30	50	45	30	130	20	30	120
13:45	35	25	20	100	20	30	130
14:00	30	50	15	145	20	60	80
14:15	35	55	15	130	20	35	70
14:30	40	40	20	70	25	30	120
14:45	45	50	15	60	35	45	70
15:00	35	30	15	70	25	40	90
15:15	50	30	30	55	25	30	80
15:30	30	45	20	120	60	45	110
15:45	30	20	20	75	15	40	90
16:00	35	45	20	180+	30	40	50
16:15	40	100	20	130	30	30	60
16:30	40	125	15	150	30	40	80
16:45	35	170	10	150	25	30	65
17:00	50	200+	10	180+	55	50	170
17:15	50	200+	150	180+	70	50	170
17:30	55	200+	40	180+	55	40	120
17:45	50	200+	75	180+	70	40	130
18:00	60	150	40	180+	50	60	130
18:15	30	40	50	135	20	30	70
18:30	40	60	20	90	30	20	30
18:45	25	40	15	60	20	20	40

Queue's are measured in meters

Cannot be seen from camera

- + Signifies queue stretches to a minimum length of x and beyond the view of the camera
- # Signifies queue stretches to the next significant junction
- * Indicates an estimated queue length due to obscured vision.



	A => A	A => B	A => C			1.21							
TIME	P/C M/C CAR LGV OGV1 OGV2 PS	TOT PCU P/C H/C CAR LOV OGV1 OGV2 P	TOT PCU P/C H/C CAR LOV OGVI OGVI PSV		0641 0642 864 101 801					C=>A	C => B		C => C
07:00	0 0 0 0 0 0		1 12 145 4 0 25 3 1 0 0			FIC HIC CAR LOV DOVI DOVI PSV	TOT PCU: P/C	C M/C CAR LEV DEVI DEV2 PSV	TOT PCU P	C M/C CAR LOV OGV1 OGV2 PSV TOT	PCU P/C H/C CAR LGV OGV1	OGV2 PSV TOT PCU	P/C H/C CAR LGV OGV1 OGV2 PSV TOT PC
02-15				33 31.8 3 0 6 3	0 0 0 12 111		0 1 0 10	0 60 12 6 0 8	96 105	1 0 6 0 0 0 0 7	6.2 10 0 45 10 1	1 2 69 69.8	0 0 0 0 0 0 0 0
07.10			0 4 43 2 0 23 6 0 0 0	31 32.4 0 0 21 7	1 0 2 31 37	0 0 0 0 0 0	0 0 0 0	2 72 12 7 0 8	107 118.5 (	0 0 15 3 0 0 0 18	19.5 9 0 47 14 0	2 4 76 82.4	0 0 0 0 0 0 0 0
07:30	0 0 0 0 0 0		1 48 52.5 0 0 46 2 0 0 0	48 49 1 0 20 5	0 0 0 26 27.7		0 0 3	0 93 19 3 4 8	130 151.8	0 0 23 1 0 0 0 24	24.5 11 0 77 7 2	0 2 99 96.7	
07:45	0 0 0 0 0 0		0 52 55.5 2 1 41 3 0 0 0	47 46.3 1 0 36 9	0 0 1 47 51.7		0 0 5	3 78 15 6 1 7	115 128 0	0 0 24 2 0 0 0 26	27 11 2 91 8 2	1 6 121 123.3	
н/тот	0 0 0 0 0 0	0 0 0 107 22 2 0	2 133 147 8 1 135 14 1 0 0	159 159.5 5 0 83 24	1 0 3 116 127.5	0 0 0 0 0 0	0 0 24	5 303 58 22 5 31	448 503.3	1 0 68 6 0 0 0 5 75	77.2 41 2 260 39 5	4 14 365 372.2	
08:00	0 0 0 0 0 0	0 0 0 1 28 5 1 0	2 37 41.4 0 1 47 0 0 0 1	49 49.4 1 0 39 4	0 0 0 44 45.2	0 0 0 0 0 0	0 0 10	2 100 13 3 2 6	136 143.4 0	0 1 23 3 0 0 0 27	27.9 14 3 90 12 1	1 1 1 122 2117.8	
08:15	0 0 0 0 0 0	0 0 0 0 38 10 1 0	0 49 54.5 1 0 57 1 1 0 0	60 60.2 1 0 39 3	1 0 1 45 47.2		0 0 0 12	3 92 11 4 5 5	132 139.6	0 0 23 1 0 0 0 3	24.6		
08:30	0 0 0 0 0 0	0 0 0 0 55 6 0 0	1 62 66 0 0 57 6 0 0 0	63 66 0 0 36 5	1 0 0 42 45			3 84 30 4 0 8				0 3 103 106.2	
08:45	0 0 0 0 0 0	0 0 0 0 0 0 0 0 0	0 66 68.5 1 0 37 4 0 0 0	42 43.2 0 0 28 3	0 0 1 12 12 145				131 139.4	0 0 39 2 2 0 0 43	45 11 2 67 10 8	2 4 124 129.6	
H/TOT	0 0 0 0 0 0 0	0 0 0 1 182 25 3 0	3 214 230.4 2 1 198 11 1 0 1	214 2218.8 2 0 142 15	2 0 2 141 1470			1 62 11 / 2 4	100 122.2	0 0 28 1 0 0 0 29	29.5 6 0 108 14 8	1 7 144 158.5	0 0 0 0 0 0 0 0 0
09:00	0 0 0 0 0 0 0		1 41 48 0 0 19 1 0 0 0					8 358 55 18 9 23	507 544.6 0	0 1 113 7 2 0 0 123	126.9 43 7 357 49 18	4 17 495 512.1	0 0 0 0 0 0 0 0 0
09:15	0 0 0 0 0 0							1 97 34 6 2 5	150 173 0	0 0 42 2 2 0 0 46	48 7 0 96 10 6	1 4 124 131.7	0 0 0 0 0 0 0 0 0
09-30				60 <b>60.6</b> 0 0 13 5	0 0 1 19 22.5		0 0 0 1	2 80 25 5 2 6	121 142.6 0	0 0 31 3 0 0 0 34	35.5 0 1 94 15 5	3 6 124 143.3	0 0 0 0 0 0 0 0
20.45				29 30.7 0 0 24 7	0 0 0 31 34.5		0 0 0 1	0 67 25 11 0 8	112 137.2 0	0 0 33 2 0 0 0 35	36 1 1 61 28 5	2 9 107 133.7	0 0 0 0 0 0 0 0
09.45	0 0 0 0 0 0		0 27 31 0 0 29 2 0 0 0	31 32 0 0 18 7	0 0 1 26 30.5	0 0 0 0 0 0	0 0 0	0 71 26 6 1 6	110 133.3 1	1 0 32 1 0 0 0 34	33.7 2 2 93 18 4	1 3 123 135.5	
н/тот	0 0 0 0 0 0	0 0 0 0 114 23 3 0	2 142 157 3 1 144 13 0 1 0	162 166.8 0 0 88 39	3 0 2 132 155		0 0 7	3 315 110 28 5 25	493 586.1 1	1 0 138 8 2 0 0 149	153.2 10 4 344 71 20	7 22 478 544.2	0 0 0 0 0 0 0 0 0
10:00	0 0 0 0 0 0	0 0 0 0 0 30 4 1 0	1 36 39.5 0 0 19 7 0 0 0	26 29.5 0 0 19 9	0 0 0 28 32.5	0 0 0 0 0 0	0 2 0 2 1	1 69 14 6 3 6	100 118.5 0	0 0 21 1 0 0 0 22	22.5 1 0 77 23 3	0 5 3 109 3 126.2	0 0 0 0 0 0 0 0
10:15	0 0 0 0 0 0	0 0 0 25 5 1 0	0 31 34 0 0 24 3 0 0 0	27 28.5 0 0 27 6	1 0 1 35 39.5	0 0 0 0 0 0	0 0 2	1 76 29 5 0 4	117 135.8	0 0 39 2 0 0 0 41	42 2 1 73 21 1	1 6 105 2121 1	
10:30	0 0 0 0 0 0	0 0 0 16 7 4 0	1 28 34.5 0 0 27 1 0 0 0	28 28.5 0 0 25 4	0 0 0 29 31		0 0 1	1 70 29 8 3 6	118 145	0 0 27 2 0 0 0 29	30 3 1 44 15 1	0 7 95 100	
10:45	0 0 0 0 0 0	0 0 0 0 20 5 1 0	0 26 29 0 0 31 2 1 0 0	34 35.5 0 0 20 3	0 0 1 24 26.5		0 0 2	2 90 32 6 4 5	141 167.4		22.5 2 1 44 15 3		
H/TOT	0 0 0 0 0 0 0	0 0 0 0 91 21 7 0	2 121 137 0 0 101 13 1 0 0	115 122 0 0 91 22	1 0 2 116 129.5	0 0 0 0 0 0	0 2 0 2 4	5 305 104 25 10 21	476 566 7	0 0 105 8 0 0	117		
11:00	0 0 0 0 0 0 0		1 22 245 0 0 32 3 1 0 0	36 38 0 0 28 3	0 0 0 31 325			A 25 23 4					
11:15	0 0 0 0 0 0	0 0 0 0 29 11 2 0	0 42 48.5 0 0 31 3 0 0 0	34 35.5 0 0 15 7	1 0 1 24 29						28 1 3 63 18 4	0 6 95 5109.4	0 0 0 0 0 0 0 0 0
11:30	0 0 0 0 0 0 0	0 0 0 29 5 0 0	1 35 38.5 0 0 27 3 0 0 0	10 11 5 0 0 21 2				3 64 30 9 0 3	132 130.3	0 0 35 0 0 0 0 35	35 2 1 76 18 6	1 5 109 125.1	0 0 0 0 0 0 0 0 0
11:45	0 0 0 0 0 0	0 0 0 21 2 1 0	0 24 255 0 0 29 3 0 0 0					2 83 30 8 3 6	134 160.1 0	0 0 23 1 1 0 0 25	26 1 2 73 17 3	1 2 99 5110.3	0 0 0 0 0 0 0 0
н/тот	0 0 0 0 0 0 0							2 90 16 8 0 7	124 141 0	0 0 25 2 2 0 0 29	31 1 2 82 21 5	2 7 120 140.6	0 0 0 0 0 0 0 0
12:00	0 0 0 0 0 0 0			142 148.3 0 0 0 00 16	1 0 2 105 115.5		0 : 0 ; 6	7 336 98 30 4 22	503 585.2 0	0 0 111 3 3 0 0 117	120 5 8 294 74 18	4 20 423 485.4	0 0 0 0 0 0 0 0 0
12.16				45 47.3 0 1 30 3	0 0 0 34 34.9		0 0 0 3	1 96 27 6 2 5	140 161.1 0	0 0 29 0 1 0 0 30	30.5 1 1 57 20 4	1 5 09 105.9	0 0 0 0 0 0 0 0
12.30			0 30 32.5 1 1 42 5 0 0 0	49 50.1 0 0 22 1	0 1 1 25 27.8		0 0 0 4	1 127 21 5 5 8	171 194.7 0	0 30 0 0 0 30	30 5 0 69 15 5	2 4 100 112.6	
12.30	0 0 0 0 0 0		1 31 34 0 0 45 1 0 0 0	46 46.5 0 0 40 3	0 0 0 43 44.5		0 0 5	1 120 17 2 1 5	151 162.2 0	0 0 35 1 0 0 0 36	36.5 3 2 72 15 2	0 5 99 108.9	
12:45	0 0 0 0 0 0		0 31 34.8 0 0 40 2 0 0 0	42 43 0 0 29 8	0 0 1 38 43		0 0 0 2	2 136 12 7 4 4	167 182.9 0	0 1 24 1 0 0 0 26	25.9 0 0 86 15 7	1 5 114 131.3	
H/TOT	0 0 0 0 0 0		2 123 135.3 1 1 167 12 1 0 0	182 187.1 0 1 121 15	0 1 2 140 150.2	0 0 0 0 0 0 0	0 2 0 2 14	5 479 77 20 12 22	629 700.9 0	0 1 118 2 1 0 0 1 122	122.9 9 3 284 65 18	4 19 402 458.7	0 0 0 0 0 0 0 0 0
13:00	0 0 0 0 0 0	0 0 0 25 2 0 0	1 28 30 1 2 38 1 0 0 0	42 40.5 0 0 58 B	0 0 0 66 70	0 0 0 0 0 0 0	0 2 0 2 3	0 140 24 8 5 4	184 208.1 0	0 0 31 3 1 0 0 35	37 5 1 0 74 17 5	0 4 3 101 3 115 2	0 0 0 0 0 0 0 0
13:15	0 0 0 0 0 0	0 0 0 0 27 1 2 0	0 30 31.5 0 0 41 7 1 0 0	49 53 0 0 27 2	1 0 1 31 33.5		0 0 1	0 92 16 7 2 7	125 145.3 0	0 0 30 1 0 0 0 31	31.5 4 1 74 12 4	2 5 102 113.8	
13:30	0 0 0 0 0 0	00000000000	1 47 51 0 0 33 1 0 0 0	34 34.5 1 0 28 3	1 0 0 33 34.2		0 0 4	0 92 25 6 2 4	133 151.9	0 0 35 1 0 0 0 14	36.5 3 3 40 21 3	1	
13:45	0 0 0 0 0 0	0 0 1 43 6 0 0	0 50 52.4 0 0 36 3 0 0 0	39 40.5 0 0 28 6	0 0 1 35 39			0 104 20 3 0 6	111 150.5				
H/TOT	0 0 0 0 0 0	0 0 0 1 135 15 2 0	2 155 164.9 1 2 148 12 1 0 0	164 168.5 1 0 141 19	2 0 2 2 165 2175.7			0 428 85 24 9 21	CTC 1655.8				
14:00	0 0 0 0 0 0	0 0 0 0 24 5 3 0	1 33 38 0 0 44 2 0 0 0	46 47 3 1 32 5	0 0 0 2 41 2 40.5			1 111 14 4 1 4				0 19 450 516.7	
14:15	0 0 0 0 0 0	0 0 0 30 5 1 0	0 36 39 0 0 48 2 0 0 0	50 51 2 1 22 5	0 0 1 31 32.3			2 1/0 10 6 3 4				1 4 94 108.6	0 0 0 0 0 0 0 0
14:30	0 0 0 0 0 0	0 0 0 0 25 9 1 0	1 36 42 0 1 36 1 0 0 0	38 37.9 0 0 26 4	0 0 0 10 10				145 101.5	0 28 2 1 0 0 29	30.5 1 3 70 13 3	1 5 96 107.7	0 0 0 0 0 0 0 0
14:45	0 0 0 0 0 0	0 0 0 29 5 0 0	0 34 365 0 0 26 4 1 0 0	11 115 0 0 14 1				3 96 24 4 0 5	133 149.4	2 0 25 1 0 0 0 28	26.9 1 0 74 14 7	2 5 103 120.3	0 0 0 0 0 0 0 0 0
H/TOT	0 0 0 0 0 0 0		2 179 155.5 0 1 154 9 1 0 0					0 85 23 7 1 4	120 140.3 0	0 0 38 6 0 0 0 44	47 1 1 84 11 6	1 4 108 2120.4	0 0 0 0 0 0 0 0
15:00								6 421 80 20 5 17	557 620.5 3	0 124 12 1 0 0 140	144.1 5 5 291 58 19	5 18 401 457	0 0 0 0 0 0 0 0
15.16				•5 •6 5 1 29 1	0 0 0 34 531.5		0 0 0 5	0 118 17 1 4 7	152 169.2 0	0 0 42 3 0 0 0 45	46.5 0 1 59 18 5	1 5 89 106.2	0 0 0 0 0 0 0 0
11.30			0 34 363 0 0 37 3 0 0 1	41 43.5 0 0 27 4	1 0 1 33 36.5		0 2 0 2 4	2 104 16 3 1 8	138 152.4 0	0 0 31 2 0 0 0 33	34 1 1 70 27 4	2 5 110 131.7	
13:30	0 0 0 0 0 0	0 0 0 29 8 0 0	1 38 43 0 0 44 2 0 0 0	46 47 1 0 44 2	0 0 0 47 47.2		0 0 5	2 106 19 7 0 8	147 162.8 1	0 36 2 0 0 0 39	39.2 3 1 69 18 1	0 2 94 102.5	
15:45	0 0 0 0 0 0 0		1 40 465 0 0 44 7 0 0 0	51 54.5 2 0 24 3	1 0 1 31 32.4		0 0 3	0 96 24 5 2 4	134 152.7 0	0 0 16 3 0 0 0 19	20.5 4 2 64 16 3	1 7 97 110.4	
н/тот	0 0 0 0 0 0	0 0 0 1 116 28 2 0	3 150 167.4 0 0 164 17 1 0 1	183 193 6 1 124 10	2 0 2 145 147.6	0 0 0 0 0 0	0 0 17	4 424 76 16 7 27	571 637.1	1 0 125 10 0 0 0 136	140.2 8 5 262 79 13	4 19 390 450.83	0 0 0 0 0 0 0 0
16:00	0 0 0 0 0 0	0 0 0 29 1 1 0	1 32 34 0 0 59 5 0 0 0	64 66.5 0 0 28 9	0 0 1 38 43.5		0 0 7	4 147 18 3 0 5	184 191.5 0	0 0 20 1 0 0 0 21	21.5 1 0 57 11 0	0 2 71 77.7	
16:15	0 0 0 0 0 0	0 0 0 0 30 8 2 0	0 40 45 0 0 57 3 0 0 0	60 61.5 0 0 28 8	0 0 1 37 42		0 0 0 5	0 119 26 2 0 5	157 172 0	0 2 19 2 1 0 0 24	24.3 3 1 60 14 2	20 2 20 20 0	
16:30	0 0 0 0 0 0	0 0 0 0 31 3 1 0	1 36 39 0 2 71 3 0 0 0	76 76.3 2 0 40 3	1 0 0 46 46.4		0 0 3	3 146 18 2 1 6	179 192 1	1 21 2 0 0 0 25	24.6 2 4 47 11 2		
16:45	0 0 0 0 0 0	0 0 0 41 4 0 0	0 45 47 1 0 54 4 0 0 0	59 60.2 0 0 37 5	0 0 1 43 46.5	0 0 0 0 0 0		1 133 22 2 2 5	173 185.6	0 15 0 0 0 0 15			
H/TOT	0 0 0 0 0 0 0	0 0 0 0 131 16 4 0	2 153 165 1 2 241 15 0 0 0	259 264.5 2 0 133 25	1 0 3 164 178.4		0 0 0 2 21	8 545 84 9 1 21	601 241 2	2 85 5 7 7 7 7			
17:00	0 0 0 0 0 0 0	0 0 0 1 36 6 0 0	1 44 47.4 0 0 52 1 0 0 0	53 53.5 3 0 50 9	0 0 0 2 62 2 64.3			5 136 2 2 2 2 2					
17:15	0 0 0 0 0 0	0 0 0 55 3 0 0	0 58 59.5 1 1 74 2 0 0 0	78 77.6 0 0 36 3	0 0 1 1 10 10					5 37 3 0 0 0 44	123 1 1 1 1 2	1 2 151 154.2	0 0 0 0 0 0 0 0
17:30	0 0 0 0 0 0	0 0 0 40 3 3 0	1 45 48 1 0 44 3 0 0 0	62 622 0 0 0			10		119 120.3	0 30 2 0 0 0 32	33 5 3 122 10 3	0 6 149 155.7	0 0 0 0 0 0 0 0 0
17:45	0 0 0 0 0 0						0 1 0 18	0 119 4 2 1 5	149 143.9	3 2 40 2 1 0 0 48	45.9 8 1 107 6 1	0 5 128 129.5	0 0 0 0 0 0 0 0
H/TOT					0 0 0 55 57.5		0 0 3 5	1 158 13 1 1 4	183 190.7 0	0 0 38 4 0 0 0 42	44 5 6 2 90 9 0	0 6 113 117.5	0 0 0 0 0 0 0 0
18.00		104 17 1 0	265 9 0 0 0	279 279.7 3 0 178 17	1 0 1 200 207.6		0 0 44	8 506 26 5 2 19	610 607.1	5 2 147 11 1 0 0 166	166.8 27 8 442 38 6	1 19 541 556.9	0 0 0 0 0 0 0 0
18:00		0 0 38 3 0 1	1 45 46.8 3 1 66 7 0 0 0	77 77.5 0 0 42 6	0 0 0 48 51	0 0 0 0 0 0	0 0 13	1 178 5 1 0 4	202 198 2	2 0 41 1 0 0 0 44	42.9 7 4 79 10 0	0 6 106 109	0 0 0 0 0 0 0 0 0
18:15		0 0 1 19 1 0 0	0 21 20.9 0 0 38 1 0 0 0	39 39.5 0 0 38 3	0 0 1 } 42 } 44.5		0 0 9	4 113 9 1 1 5	142 143.7 2	2 0 45 3 0 0 0 50	49.9 3 0 72 3 1	0 6 85 90.6	
18:30	0 0 0 0 0 0	0 0 2 19 1 0 0	1 23 23.3 1 0 45 3 0 0 0	49 49.7 0 0 25 0	0 0 0 25 25		0 0 5	0 107 2 1 0 4	119 120.5	2 1 31 2 0 0 0 36	34.8 9 0 82 3 0	0 7 101 102.3	
18:45	0 0 0 0 0 0	2 0 2 0 2 0 0 29 3 0 0	1 33 35.5 2 1 44 5 0 0 0	52 52.3 0 0 19 0	0 0 1 20 21	0 0 0 0 0 0	0 0 0 0	0 82 7 0 1 5	95 104.8	0 26 0 0 0 26	26 8 1 97 2 0	0 8 116 118	0 0 0 0 0 0 0 0
н/тот	0 0 0 0 0 0	0 0 0 3 105 8 0 1	3 120 126.5 6 2 193 16 0 0 0	217 219 0 0 124 9	0 0 2 135 141.5	0 0 0 0 0 0 0	0 0 27	5 480 23 3 2 18	558 : 567 : 6	5 1 143 6 0 0 0 1 156	153.6.2 27 5 330 18 1	0 27 408 419.9	
12 TOT	0 0 0 0 0 0	0 0 0 7 1452 235 35 2 3	27 1758 1918 26 12 2039 153 8 1 2	2241 2297 24 4 1415 228	16 1 25 1713 1840	0 0 0 0 0 0 0	0 : 0 : 220	64 4900 876 220 73 267	6620 7316	8 8 1413 86 13 0 0 5 1510	1568 203 58 3729 673 151	43 233 5000 5000	
				***************************************		······						2	



# **TRICS Output Data**

MH21009 | Large-scale Residential Development 'Swift Square Apartments' | F01 | July 2023 rpsgroup.com JBBarry & Partners Monastery Road Dublin

#### TRIP RATE for Land Use 03 - RESIDENTIAL/C - FLATS PRIVATELY OWNED TOTAL VEHICLES Calculation factor: 1 TOTBED Estimated TRIP rate value per 380 TOTBED shown in shaded columns BOLD print indicates peak (busiest) period

	ARRIVALS					DEP	ARTURES		TOTALS					
Time Range	No. Days	Ave. TOTBED	Trip Rate	Estimated Trip Rate	No. Davs	Ave. TOTBED	Trip Rate	Estimated Trip Rate	No. Davs	Ave. TOTBED	Trip	Estimated		
00:00 - 01:00					/-			inp nate	00/0	101020	Hute	Thp Rate		
01:00 - 02:00														
02:00 - 03:00														
03:00 - 04:00														
04:00 - 05:00														
05:00 - 06:00														
06:00 - 07:00														
07:00 - 08:00	46	122	0.021	8.141	46	122	0.079	29.852	46	122	0.100	37,993		
08:00 - 09:00	46	122	0.034	12.755	46	122	0.099	37.586	46	122	0.133	50.341		
09:00 - 10:00	46	122	0.042	15.944	46	122	0.045	17.029	46	122	0.087	32,973		
10:00 - 11:00	46	122	0.036	13.569	46	122	0.044	16.893	46	122	0.080	30,462		
11:00 - 12:00	46	122	0.036	13.705	46	122	0.044	16.826	46	122	0.080	30.531		
12:00 - 13:00	46	122	0.047	17.911	46	122	0.045	17.233	46	122	0.092	35.144		
13:00 - 14:00	46	122	0.040	15.062	46	122	0.047	17,708	46	122	0.087	32,770		
14:00 - 15:00	46	122	0.044	16.554	46	122	0.046	17.436	46	122	0.090	33,990		
15:00 - 16:00	46	122	0.055	20.964	46	122	0.037	14.247	46	122	0.092	35.211		
00 - 17:00	46	122	0.068	25.917	46	122	0.043	16.283	46	122	0.111	42,200		
00 - 18:00	46	122	0.091	34.601	46	122	0.048	18.115	46	122	0.139	52.716		
18:00 - 19:00	46	122	0.079	30.055	46	122	0.054	20.421	46	122	0.133	50.476		
19:00 - 20:00														
20:00 - 21:00														
21:00 - 22:00														
22:00 - 23:00														
23:00 - 24:00														
Total Rates:			0.593	225.178			0.631	239.629			1.224	464.807		

This section displays the trip rate results based on the selected set of surveys and the selected count type (shown just above the table). It is split by three main columns, representing arrivals trips, departures trips, and total trips (arrivals plus departures). Within each of these main columns are three sub-columns. These display the number of survey days where count data is included (per time period), the average value of the selected trip rate calculation parameter (per time period), and the trip rate result (per time period). Total trip rates (the sum of the column) are also displayed at the foot of the table.

To obtain a trip rate, the average (mean) trip rate parameter value (TRP) is first calculated for all selected survey days that have count data available for the stated time period. The average (mean) number of arrivals, departures or totals (whichever applies) is also calculated (COUNT) for all selected survey days that have count data available for the stated time period. Then, the average count is divided by the average trip rate parameter value, and multiplied by the stated calculation factor (shown just above the table and abbreviated here as FACT). So, the method is: COUNT/TRP*FACT. Trip rates are then rounded to 3 decimal places.

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#### Parameter summary

Trip rate parameter range selected:	21 - 725 (units: )
Survey date date range:	01/01/14 - 15/10/21
Number of weekdays (Monday-Friday):	46
Number of Saturdays:	0
Number of Sundays:	0
Surveys automatically removed from selection:	0
Surveys manually removed from selection:	0

This section displays a quick summary of some of the data filtering selections made by the TRICS® user. The trip rate calculation parameter range of all selected surveys is displayed first, followed by the range of minimum and maximum survey dates selected by the user. Then, the total number of selected weekdays and weekend days in the selected set of surveys are show. Finally, the number of survey days that have been manually removed from the selected set outside of the standard filtering procedure are displayed.

JBBarry & Partners Monastery Road Dublin

#### TRIP RATE for Land Use 02 - EMPLOYMENT/A - OFFICE **TOTAL VEHICLES Calculation factor: 100 sqm** Estimated TRIP rate value per 14222 SQM shown in shaded columns BOLD print indicates peak (busiest) period

		AR	RIVALS			DEP	ARTURES		TOTALS					
Time Range	No. Days	Ave. GFA	Trip Rate	Estimated Trip Rate	No. Days	Ave. GFA	Trip Rate	Estimated Trip Rate	No. Days	Ave. GFA	Trip Rate	Estimated Trip Rate		
00:00 - 01:00														
01:00 - 02:00														
02:00 - 03:00														
03:00 - 04:00														
04:00 - 05:00														
05:00 - 06:00														
06:00 - 07:00	1	10100	1.109	157.709	1	10100	0.168	23.938	1	10100	1.277	181.647		
07:00 - 08:00	51	3211	0.503	71.483	51	3211	0.061	8.686	51	3211	0.564	80.169		
08:00 - 09:00	54	3154	1.150	163.592	54	3154	0.127	18.038	54	3154	1.277	181.630		
09:00 - 10:00	54	3154	0.624	88.686	54	3154	0.180	25.553	54	3154	0.804	114.239		
10:00 - 11:00	54	3154	0.245	34.906	54	3154	0.164	23.299	54	3154	0.409	58.205		
11:00 - 12:00	54	3154	0.168	23.883	54	3154	0.163	23.132	54	3154	0.331	47.015		
12:00 - 13:00	54	3154	0.218	31.065	54	3154	0.338	48.017	54	3154	0.556	79.082		
13:00 - 14:00	54	3154	0.293	41.671	54	3154	0.288	40.919	54	3154	0.581	82.590		
14:00 - 15:00	54	3154	0.181	25.804	54	3154	0.251	35.741	54	3154	0.432	61.545		
15:00 - 16:00	54	3154	0.136	19.374	54	3154	0.359	51.107	54	3154	0.495	70.481		
16:00 - 17:00	54	3154	0.149	21.128	54	3154	0.638	90.773	54	3154	0.787	111.901		
17:00 - 18:00	54	3154	0.100	14.196	54	3154	0.899	127.851	54	3154	0.999	142.047		
18:00 - 19:00	51	3303	0.048	6.838	51	3303	0.354	50.402	51	3303	0.402	57.240		
19:00 - 20:00	1	1820	0.000	0.000	1	1820	0.000	0.000	1	1820	0.000	0.000		
20:00 - 21:00	1	1820	0.000	0.000	1	1820	0.055	7.814	1	1820	0.055	7.814		
21:00 - 22:00														
22:00 - 23:00														
23:00 - 24:00														
Total Rates:			4.924	700.335			4.045	575.270			8.969	1275.605		

This section displays the trip rate results based on the selected set of surveys and the selected count type (shown just above the table). It is split by three main columns, representing arrivals trips, departures trips, and total trips (arrivals plus departures). Within each of these main columns are three sub-columns. These display the number of survey days where count data is included (per time period), the average value of the selected trip rate calculation parameter (per time period), and the trip rate result (per time period). Total trip rates (the sum of the column) are also displayed at the foot of the table.

To obtain a trip rate, the average (mean) trip rate parameter value (TRP) is first calculated for all selected survey days that have count data available for the stated time period. The average (mean) number of arrivals, departures or totals (whichever applies) is also calculated (COUNT) for all selected survey days that have count data available for the stated time period. Then, the average count is divided by the average trip rate parameter value, and multiplied by the stated calculation factor (shown just above the table and abbreviated here as FACT). So, the method is: COUNT/TRP*FACT. Trip rates are then rounded to 3 decimal places.

JBBarry & Partners Monastery Road Dublin

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#### Parameter summary

Trip rate parameter range selected:	118 - 15000 (units: sqm)
Survey date date range:	01/01/15 - 23/11/22
Number of weekdays (Monday-Friday):	54
Number of Saturdays:	0
Number of Sundays:	0
Surveys automatically removed from selection:	2
Surveys manually removed from selection:	0

This section displays a quick summary of some of the data filtering selections made by the TRICS® user. The trip rate calculation parameter range of all selected surveys is displayed first, followed by the range of minimum and maximum survey dates selected by the user. Then, the total number of selected weekdays and weekend days in the selected set of surveys are show. Finally, the number of survey days that have been manually removed from the selected set outside of the standard filtering procedure are displayed.



# **Traffic and Transport Assessment**

MH21009 | Large-scale Residential Development 'Swift Square Apartments' | F01 | July 2023 rpsgroup.com JOM Investments Unlimited Company

# Proposed Large-Scale Residential Development 'Swift Square Apartments'

**Traffic and Transport Assessment** 



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# **Document Control Sheet**

Client:	JOM Investments Unlimited Company
Project Title:	Proposed Large-Scale Residential Development 'Swift Square Apartments'
Document Title:	Traffic and Transport Assessment
File Name:	21204-JBB-00-ZZ -RP-C-00001_TTA - Traffic and Transport Assessment

Table of Contents	List of Tables	List of Figures	Pages of Text	Appendices
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Υ	Ν	Ν	42	2 no.

Document Revision				Document Verification					
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Add hyperlink to Verification Email on PIM Register for each issue									
23-09-2021	P01	S03	AG/GC	GC	GF	GF			
11-10-2022	P02	S03	KCL	AM	GF	GF			
27-10-2022	P03	S03	KCL	AM	GF	GF			
03-11-2022	P04	S03	KCL	AM	GF	GF			
09-02-2023	P05	S03	KCL	AM	GF	GF			
24-04-2023	P06	S03	KCL	AM	GF	GF			
12-05-2023	P07	S03	KCL	KCL	GF	GF			
27-06-2023	P08	S03	KCL	KCL	GF	GF			



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### APPENDIX 1 – TRAFFIC COUNT DATA APPENDIX 2 – TRICS OUTPUT FILES



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# SECTION 1: INTRODUCTION

# 1.1 Background

J.B. Barry & Partners Ltd. was commissioned by JOM Investments Unlimited Company to prepare a Traffic & Transport Assessment (TTA) for a proposed large-scale residential development at Swift Square, Northwood, Dublin 9.

In summary, the proposed development will consist of the following:

- Site clearance, including the removal of all structures on site part of existing surface car parking;
- Relocation of existing surface car parking spaces catering for Swift Square Office Park personnel to the new basement accessible via a new ramp off the local road from Northwood Avenue, and the new undercroft parking area with access at street level off the local road to the north of the site;
- Construction of 3 no. apartment blocks (1, 2 and 3) over a partially shared podium structure, with heights ranging from 4 to 9 storeys, comprising 192 no. apartment units (4 no. 1-bedroom units and 188 no. 2-bedroom units), ancillary residential uses and associated car and bicycle parking; and
- Provision of public and communal open spaces, public realm, boundary treatments, landscaping and lighting; refuse storage, associated drainage, attenuation and services; temporary car parking area, construction access, and basement access route and ramp; and all associated site development works.

A detailed description of the proposed development is provided in the Planning Report prepared by RPS and enclosed with the submission package.

# 1.2 Consultation and Scoping Study

Section 247 meetings were held on the 01st Sept 2022 and 24th June 2022 with Fingal County Council (FCC) to discuss the development including the study area and agree the traffic junctions under consideration for this TTA. To determine current traffic behaviour in the vicinity of the subject site, it was agreed with Fingal County Council that a vehicle turning movement survey would include seven junctions surrounding the proposed development:

- Site 1- Junction 1) Ballymun Road (R108) / St. Margaret's Road;
- Site 2- Junction 2) Ballymun Road (R108) / Northwood Avenue;
- Site 3- Junction 3) Northwood Avenue / Old Ballymun Road;
- Site 4- Junction 4) Northwood Avenue / Access Road to Gulliver's Retail Park;
- Site 5- Junction 5) Northwood Avenue / Northwood Road;
- Site 6- Junction 6) Santry Avenue / Northwood Road; and
- Site 7- Junction 7) Northwood Avenue / Swords Road (R138).

These junctions were selected as they are considered the junctions mostly likely to be affected by traffic associated with the proposed development. The location of these seven junctions have been illustrated in **Figure 9** below (Page 12).

### 1.3 Objectives

This report provides an assessment of the potential traffic impacts associated with the proposed development. In this regard, the assessment aims to:



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- Identify the existing environment in terms of traffic, existing transport infrastructure and emerging transport developments;
- Quantify the likely vehicle traffic flows to and from the development onto the surrounding road network;
- Identify and quantify the likely traffic impacts on the surrounding road network resulting from the development;
- Identify any potential impacts on vulnerable road users in the study area;
- Produce a car and bicycle parking strategy; and
- Identify suitable measures to mitigate traffic and transportation impacts, if any, associated directly with the development.

The assessment is based on the findings of site visits, traffic observations, on-site traffic counts, architectural plans, discussions with the Design Team and consultation with FCC.

## 1.4 Methodology

The methodology adopted for this report is summarised as follows:

- A site audit was undertaken to quantify existing road network issues and identify local infrastructure characteristics, in addition to establishing the level of accessibility to the Site in terms of walking, cycling and public transport;
- Reference was made to site layout drawings;
- Existing and proposed access arrangements for the proposed development onto Northwood Avenue were considered;
- Historical traffic surveys were obtained (from Tuesday, 12th February 2019), at the junctions most likely to be impacted by the proposed development;
- A trip generation exercise has been carried out to establish the potential level of vehicle trips generated by the proposed development;
- In accordance with the Traffic and Transport Assessment Guidelines (2014), the specific level of influence generated by the proposed development upon the surrounding local road network was ascertained and the junctions which required assessment in greater detail were identified; and
- The junctions considered most likely to be impacted upon by traffic movements associated with the development were assessed in terms of capacity.

In preparing this assessment, reference has been made to the following documents:

- Traffic and Transport Assessment Guidelines (2014) as published by the former National Roads Authority (NRA) now Transport Infrastructure Ireland (TII);
- Traffic Management Guidelines (2019) as published by the Department of Transport, Tourism and Sport;
- TII PE-PAG-02017 Project Appraisal Guidelines for National Roads Unit 5.3 Travel Demand Projections (2021) as published by the former NRA now TII;
- Design Manual for Urban Roads and Streets (DMURS) (2013 and updated in 2022) as published by the Department of Transport;
- Fingal Development Plan 2017-2023 and Fingal Development Plan 2023-2029 as published by the Fingal County Council;
- Design Standards for New Apartments, Guidelines for Planning Authorities (2015 and updated in 2020) as published by the Department of Housing, Local Government and Heritage;
- Guidelines on the information to be contained in Environmental Impact Assessment Reports (2022) as published by the Environmental Protection Agency (EPA);



- Sustainable Mobility Policy Action Plan 2022 2025 as published by the Department of Transport;
- Greater Dublin Area (GDA) Transport Strategy 2022 2042 as published by the National Transport Authority (NTA);
- Greater Dublin Area Cycle Network Plan (2013) as published by the NTA; and
- Sustainable Urban Housing: Design Standards for New Apartments (2020) as published by the Department of Housing, Local Government and Heritage.



# SECTION 2: RECEIVING ENVIRONMENT

# 2.1 Site Location

The proposed development site is located in the Northwood area, in Dublin 9. Figure 1 and Figure 2 below illustrates the location and setting of the proposed development.



Figure 1: Location of the Proposed Development (indicative subject Site outline in red) (Source: Google Maps, annotation by J.B. Barry & Partners)



Figure 2: Location and Setting of the Proposed Development within the Northwood Area (indicative subject Site outline in red) (Source: Google Maps, annotation by J.B. Barry & Partners)



# 2.2 Land Use & Local Road Network

The existing Site is currently used as surface car parking area associated with the Swift Square Park Office buildings and temporary parking facilitating construction workers at Blackwood Square Strategy Housing Development (SHD) (ABP-306075-19) to the west of the subject Site. Vehicular access is currently connected to a sideroad Cedarview and vehicles can travel to Northwood Avenue from the existing carpark via Cedarview and the local access road to the west of the Site. The Site is bounded by Swift Square Office Park development to the south, Cedarview residential development to the north, local access road and Gulliver's Retail Park to the west, and the Whitehaven SHD to the south-east.

The land uses surrounding the development site are a mix of commercial, healthcare and residential (comprising both individual dwellings and larger residential apartment blocks), all of which benefit from access to / from Northwood Avenue.

The Site is zoned "ME-Metro Economic Corridor" within the Fingal Development Plan 2023-2029 with an objective description:

"Facilitate opportunities for high-density mixed-use employment generating activity and commercial development, and support the provision of an appropriate quantum of residential development within the Metro Economic Corridor"

The Zoning objective vision states;

"Provide for an area of compact, high intensity/density, employment generating activity with associated commercial and residential development which focuses on the Metro within a setting of exemplary urban design, public realm streets and places, which are permeable, secure and within a high-quality green landscape. Landmark buildings will provide strong quality architectural features, which respect and enhance the character of the area into which they sit. The designated areas will form sustainable districts which possess a high degree of connectivity and accessibility and will be developed in a phased manner subject to the necessary provision of social and physical infrastructure."

### 2.3 Sustainable Transport

An audit of the existing and proposed facilities and nearby transport was undertaken for the development site in the course of developing this Traffic and Transport Assessment. The proposed development is located approximately 600 metres to the south of M50, allowing easy access to and from the area by car from outer areas. The Site of the proposed development is located close to a number of bus routes and a number of emerging transport developments. The audit considered the quality and availability of the existing facilities and public transport services. The audit found that the subject Site and surrounding lands are currently very well serviced by public transport.

The existing public transport facilities and emerging transport developments in the area surrounding the Northwood area are detailed following.

#### Pedestrian and Cycle Infrastructure

As a modern development, the pedestrian and cycle facilities within the Northwood area are of a good quality. All pedestrian routes leading to / from the development benefit from the provision of street lighting in addition to good quality pedestrian footways. There are numerous pedestrians crossing facilities available along Northwood Avenue just south of the development. Additionally, off road cycle tracks are provided throughout the Northwood area and on the external road network. Ballymun Road has an off-road cycle track while Swords Road has an On-Road cycle track. **Figure 3** below illustrates the existing cycle network in the area and **Figure 4** illustrates the proposed improvements from the NTA's "Greater Dublin Area Cycle Network Plan (2013)". The off-road cycle lane along Northwood Avenue branches out at numerous locations

